

# Fluid Mechanics - MTF053

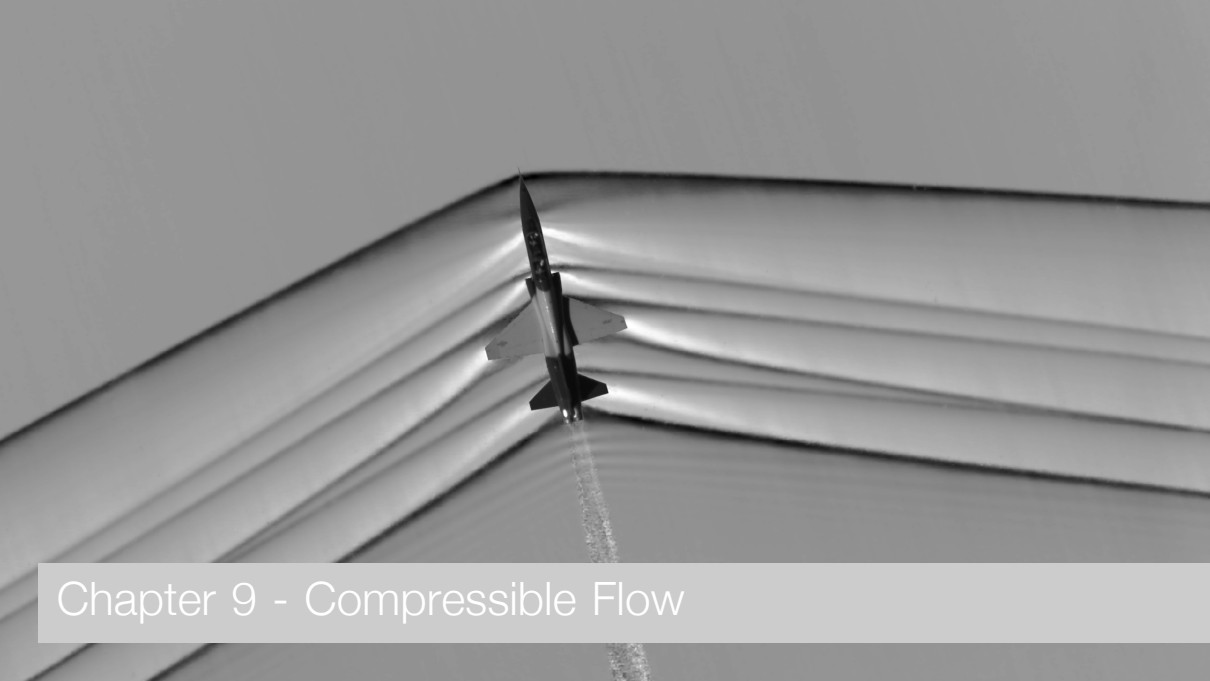
## Lecture 20

Niklas Andersson

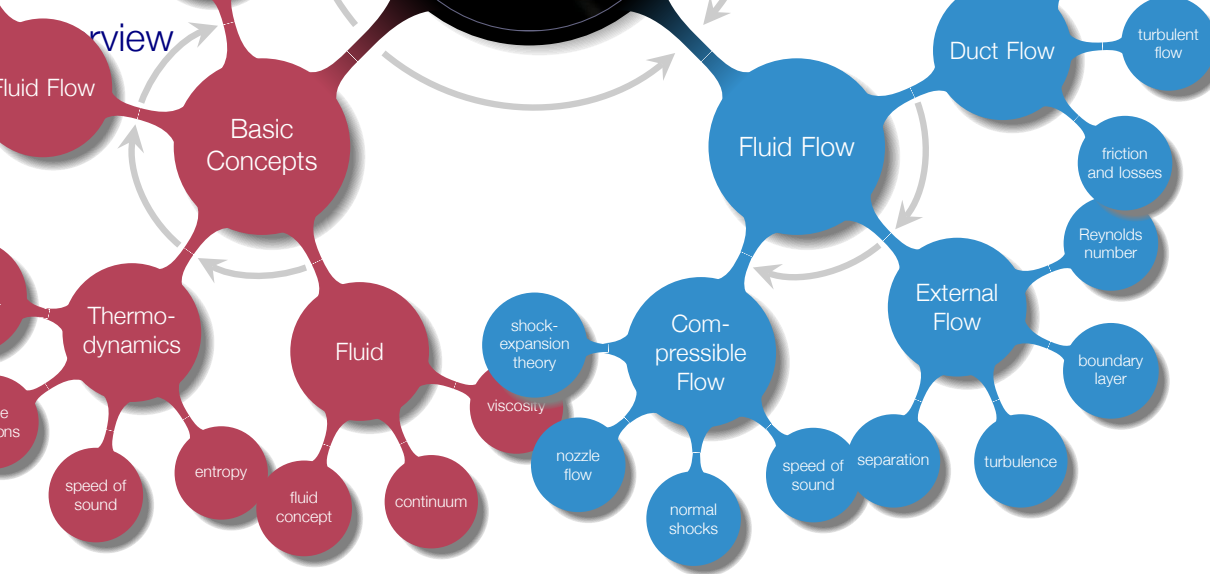
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## Chapter 9 - Compressible Flow

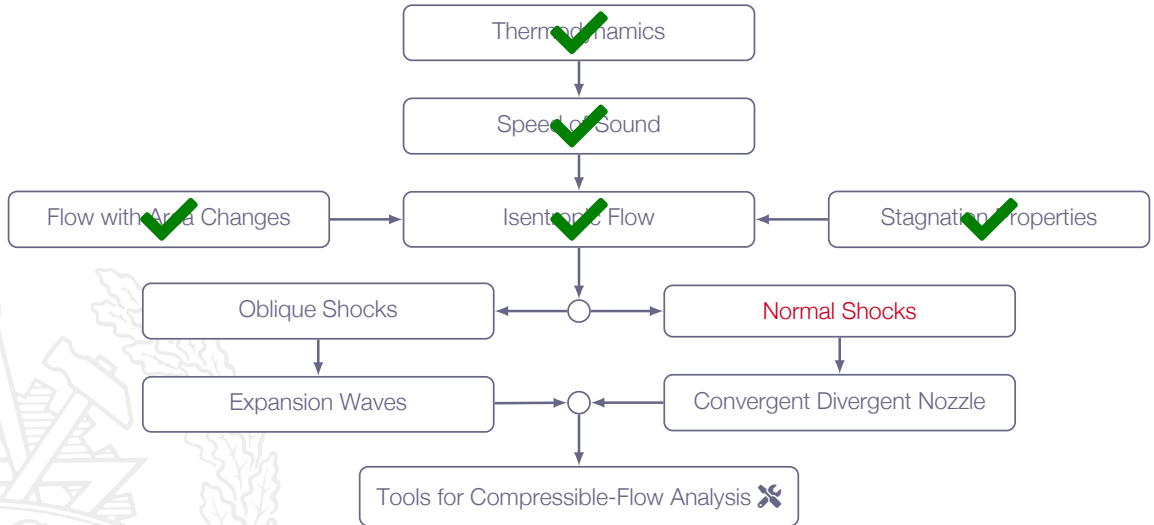


# Learning Outcomes

- 4 Be **able to categorize** a flow and **have knowledge about** how to select applicable methods for the analysis of a specific flow based on category
- 37 **Understand and explain** basic concepts of compressible flows (the gas law, speed of sound, Mach number, isentropic flow with changing area, normal shocks, oblique shocks, Prandtl-Meyer expansion)

*Let's go supersonic ...*

# Roadmap - Compressible Flow



# Shock Waves

*"Shock waves are nearly discontinuous changes in a supersonic flow"*

Reasons for the appearance of shocks in a flow can be for example:

1. higher downstream pressure
2. sudden changes in flow direction
3. blockage by a downstream body
4. explosion

# Normal Shocks

Continuity:

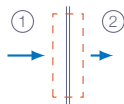
$$\rho_1 u_1 = \rho_2 u_2$$

Momentum:

$$p_1 - p_2 = \rho_2 u_2^2 - \rho_1 u_1^2$$

Energy:

$$h_1 + \frac{1}{2}u_1^2 = h_2 + \frac{1}{2}u_2^2 = h_o$$



The Rankine-Hugoniot relation:

$$h_2 - h_1 = \frac{1}{2}(p_2 - p_1) \left( \frac{1}{\rho_2} + \frac{1}{\rho_1} \right)$$

# Normal Shocks

$$h_2 - h_1 = \frac{1}{2}(p_2 - p_1) \left( \frac{1}{\rho_2} + \frac{1}{\rho_1} \right)$$

**Note!** The **Rankine-Hugoniot** relation **only** includes **thermodynamic properties** (no velocities) and gives a relation between the flow state upstream of the shock and the flow downstream of the shock



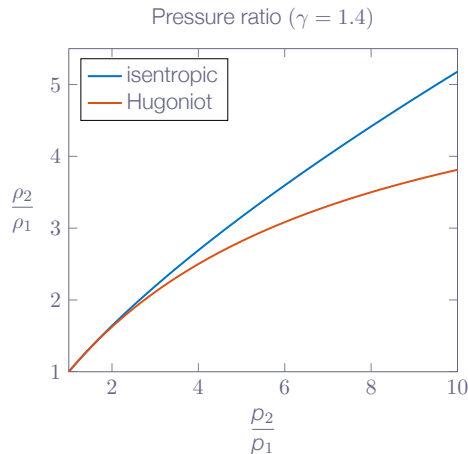
# Normal Shocks

## The Rankine-Hugoniot relation

$$\frac{\rho_2}{\rho_1} = \frac{1 + \left(\frac{\gamma+1}{\gamma-1}\right) \left(\frac{p_2}{p_1}\right)}{\left(\frac{\gamma+1}{\gamma-1}\right) + \left(\frac{p_2}{p_1}\right)}$$

## The isentropic relation

$$\frac{\rho_2}{\rho_1} = \left(\frac{p_2}{p_1}\right)^{1/\gamma}$$



# Normal Shocks

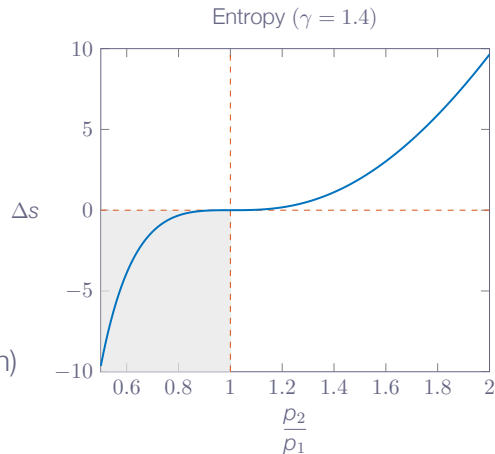
The second law of thermodynamics

$$s_2 - s_1 = C_p \ln \frac{T_2}{T_1} - R \ln \frac{p_2}{p_1}$$

can be rewritten as

$$s_2 - s_1 = C_v \ln \left[ \frac{p_2}{p_1} \left( \frac{\rho_1}{\rho_2} \right)^\gamma \right]$$

( $\rho_2/\rho_1$  from the Rankine-Hugoniot relation)



**Note!** a reduction of entropy is a violation of the second law of thermodynamics

# Normal Shocks

For a perfect gas, it is possible to obtain relations for normal shocks that only include upstream variables

Momentum equation:  $p_1 + \rho_1 u_1^2 = p_2 + \rho_2 u_2^2$

$$p_2 - p_1 = \rho_1 u_1^2 - \rho_2 u_2^2 = \{\rho_1 u_1 = \rho_2 u_2\} = \rho_1 u_1 (u_1 - u_2) = \rho_1 u_1^2 \left(1 - \frac{u_2}{u_1}\right)$$

divide by  $p_1$

$$\frac{p_2}{p_1} = 1 + \frac{\rho_1 u_1^2}{p_1} \left(1 - \frac{u_2}{u_1}\right)$$

$$u_1^2 = M_1^2 a_1^2 = M_1^2 \gamma R T_1 = \gamma M_1^2 \frac{p_1}{\rho_1} \Rightarrow \frac{p_2}{p_1} = 1 + \gamma M_1^2 \left(1 - \frac{u_2}{u_1}\right)$$

# Normal Shocks

$$\frac{p_2}{p_1} = 1 + \gamma M_1^2 \left( 1 - \frac{u_2}{u_1} \right)$$

Using the energy equation its possible obtain a relation for  $\frac{u_2}{u_1}$   
(the derivation is quite lengthy though)

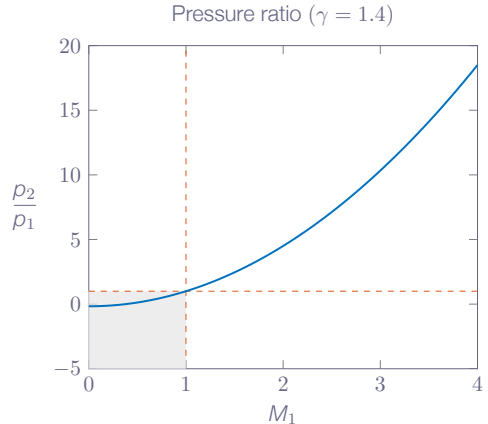
$$\frac{u_2}{u_1} = \frac{2 + (\gamma - 1)M_1^2}{(\gamma + 1)M_1^2}$$

and thus

$$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma + 1} (M_1^2 - 1)$$

# Normal Shocks

$$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma + 1} (M_1^2 - 1)$$



**Note!** from before we know that  $p_2/p_1$  must be greater than 1.0, which means that  $M_1$  must be greater than 1.0

# Normal Shocks

Momentum equation:  $p_1 + \rho_1 u_1^2 = p_2 + \rho_2 u_2^2$

$$M = \frac{u}{a} \Rightarrow p_1 + \rho_1 M_1^2 a_1^2 = p_2 + \rho_2 M_2^2 a_2^2$$

$$a = \sqrt{\gamma R T} = \sqrt{\frac{\gamma p}{\rho}} \Rightarrow p_1 + \rho_1 M_1^2 \frac{\gamma p_1}{\rho_1} = p_2 + \rho_2 M_2^2 \frac{\gamma p_2}{\rho_2}$$

$$p_1 (1 + \gamma M_1^2) = p_2 (1 + \gamma M_2^2)$$

$$\frac{p_2}{p_1} = \frac{1 + \gamma M_1^2}{1 + \gamma M_2^2}$$

# Normal Shocks

Two ways to calculate the pressure ratio over the shock

$$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma + 1} (M_1^2 - 1)$$

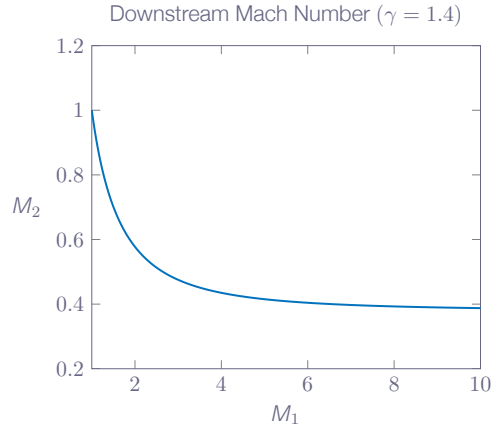
$$\frac{p_2}{p_1} = \frac{1 + \gamma M_1^2}{1 + \gamma M_2^2}$$

Setting the relations equal gives a relation for the downstream Mach number

$$M_2^2 = \frac{(\gamma - 1)M_1^2 + 2}{2\gamma M_1^2 - (\gamma - 1)}$$

# Normal Shocks

$$M_2^2 = \frac{(\gamma - 1)M_1^2 + 2}{2\gamma M_1^2 - (\gamma - 1)}$$



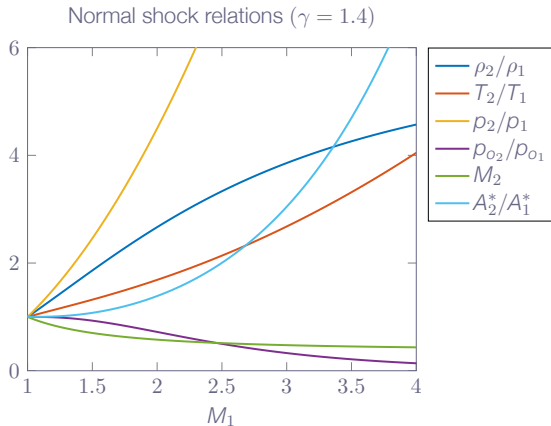
**Note!** for  $\gamma > 1$  and  $M_1 > 1$ , the downstream Mach number **must** be less than 1.0, i.e we will **always** have subsonic flow downstream of a normal shock



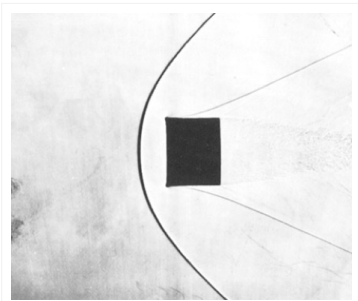
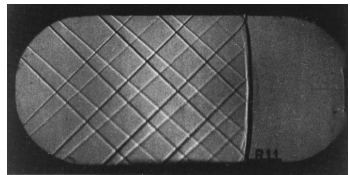
# Normal Shocks - Summary

1. **Supersonic** flow **upstream** of normal shock
2. **Subsonic** flow **downstream** of normal shock
3. **Entropy increases** over the shock and consequently **total pressure decreases**
4. Sonic throat area increases
5. Very weak shock waves are nearly isentropic

# Normal Shocks - Trends



# Normal Shocks - Examples

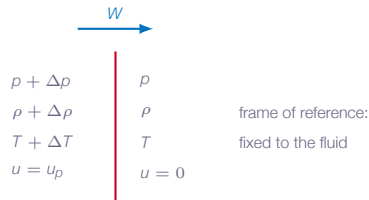


# Moving Normal Shocks

Change **frame of reference**:

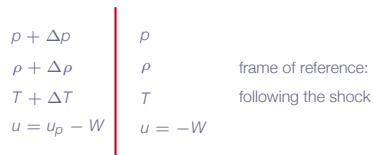
1. coordinate system moving with the shock
2. thermodynamic properties does not change

$$h_2 - h_1 = \frac{1}{2}(p_2 - p_1) \left( \frac{1}{\rho_1} + \frac{1}{\rho_2} \right)$$



$\rho + \Delta\rho$	$\rho$
$\rho + \Delta\rho$	$\rho$
$T + \Delta T$	$T$
$u = u_p$	$u = 0$

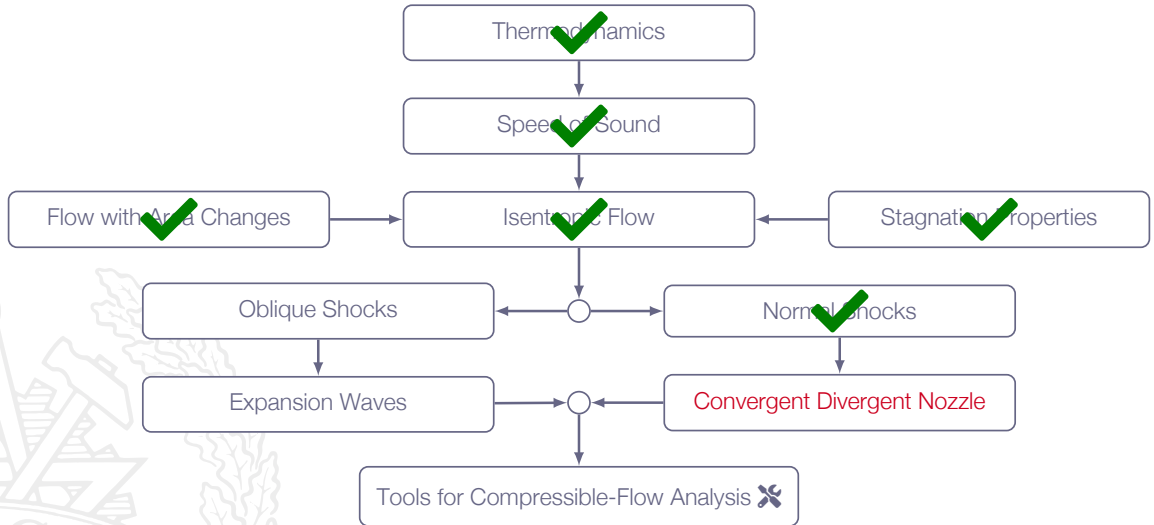
frame of reference:  
fixed to the fluid



$\rho + \Delta\rho$	$\rho$
$\rho + \Delta\rho$	$\rho$
$T + \Delta T$	$T$
$u = u_p - W$	$u = -W$

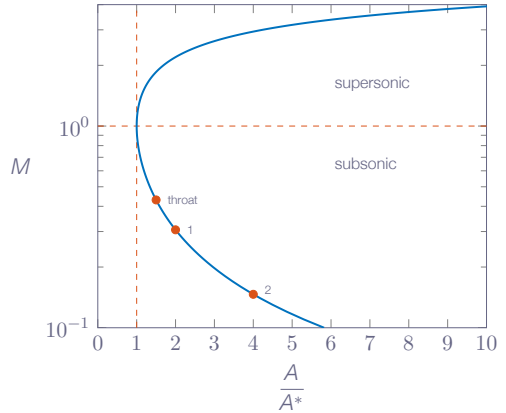
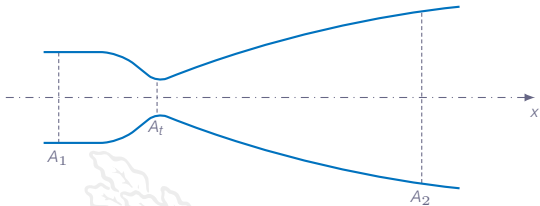
frame of reference:  
following the shock

# Roadmap - Compressible Flow



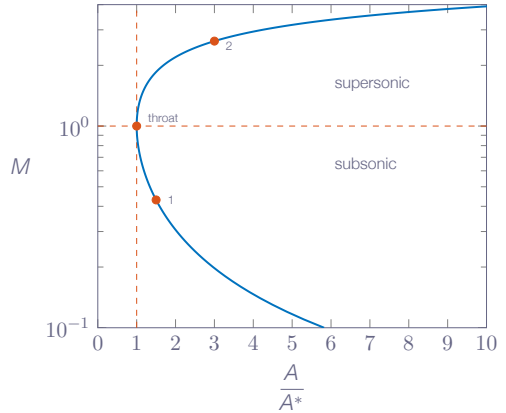
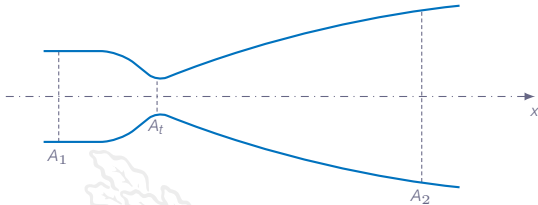
# The Area-Mach-Number Relation

Sub-critical (**non-choked**) nozzle flow

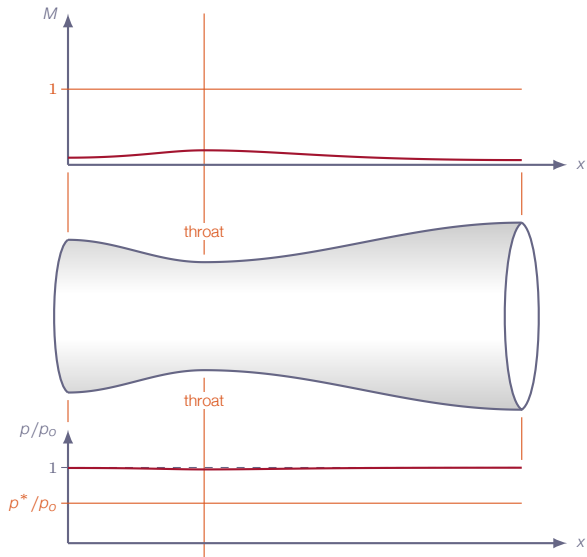
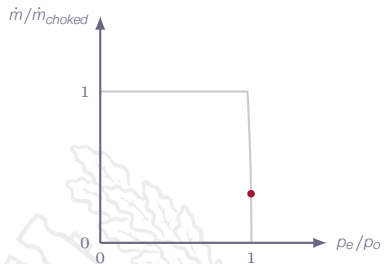


# The Area-Mach-Number Relation

Critical (**choked**) nozzle flow

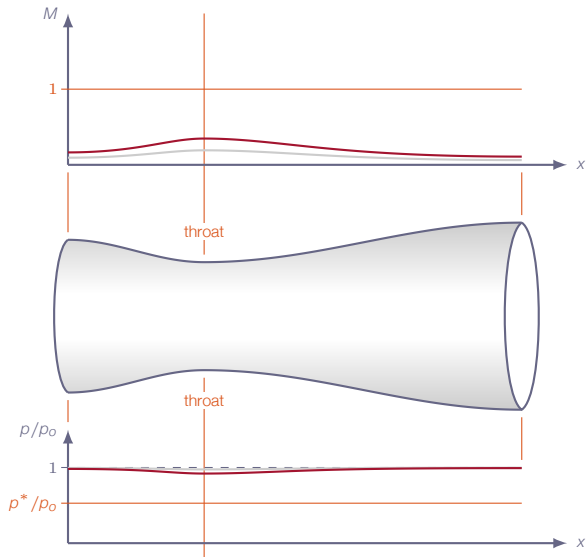
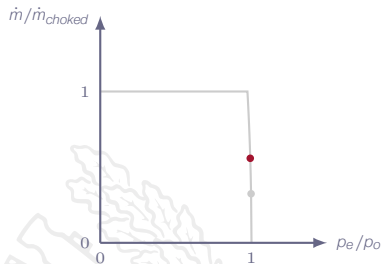


# Convergent-Divergent Nozzle

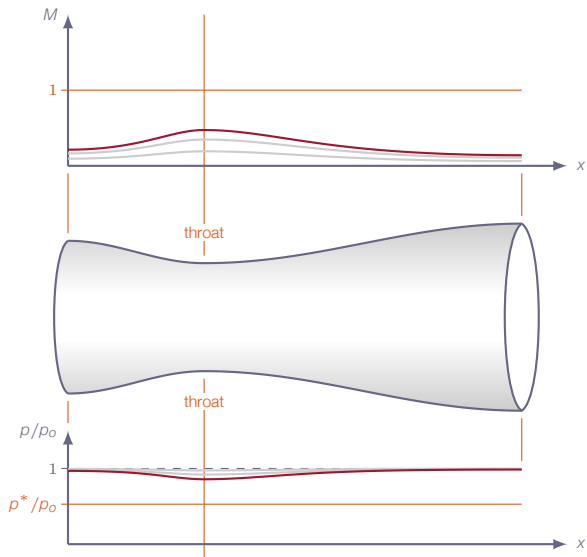
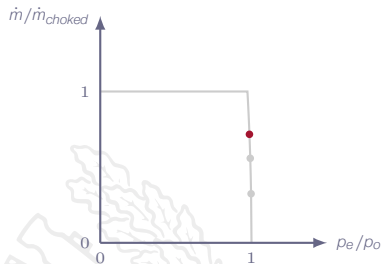




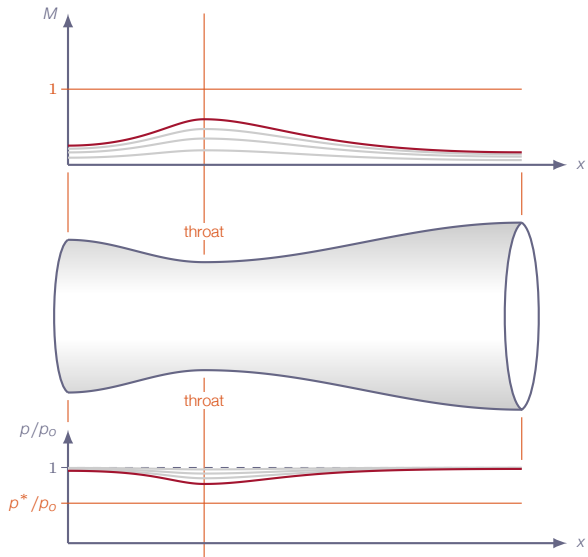
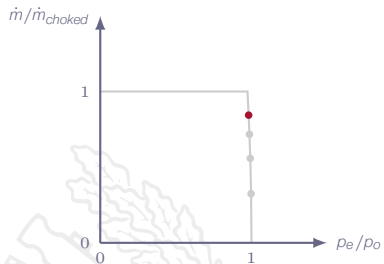
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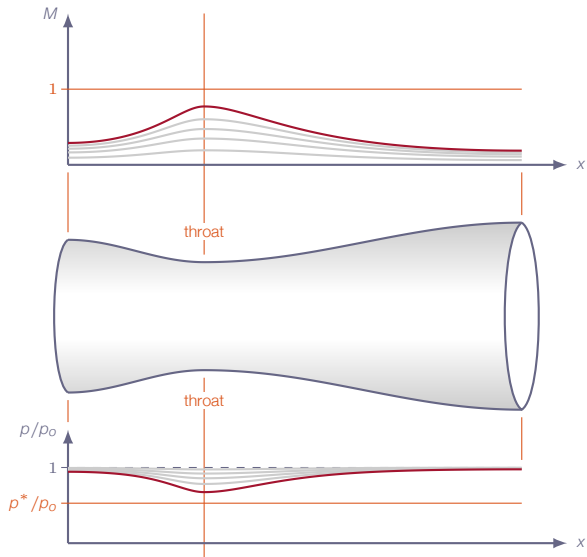
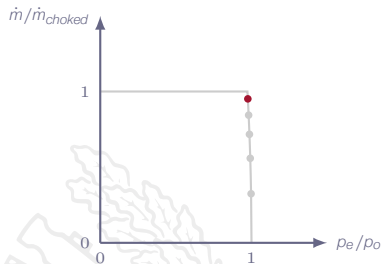
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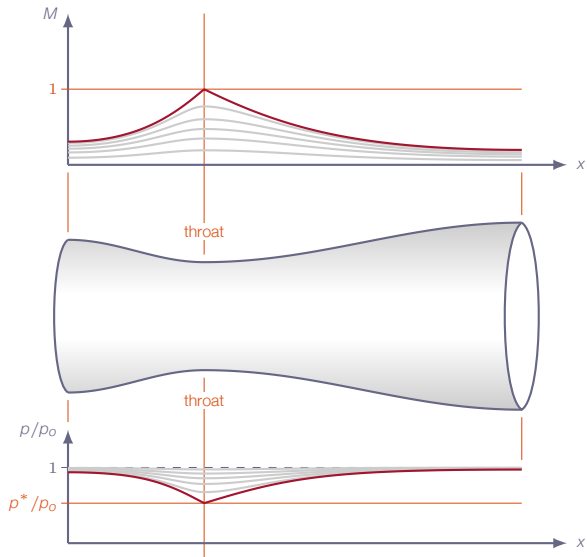
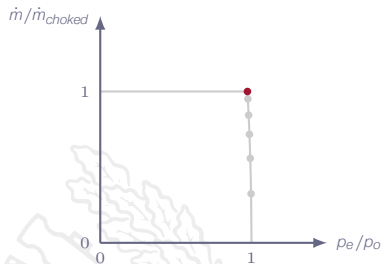
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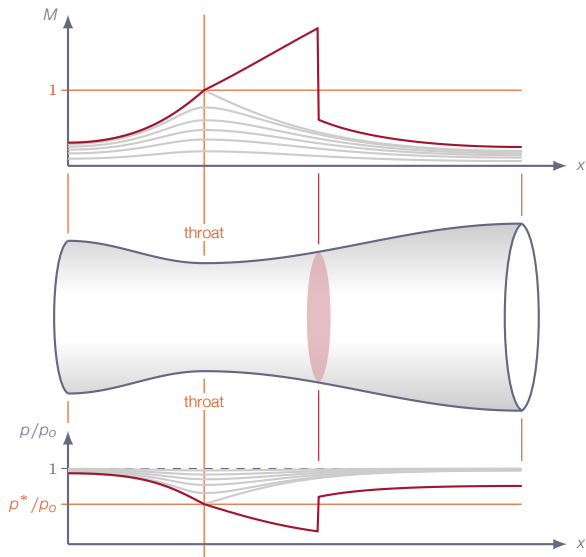
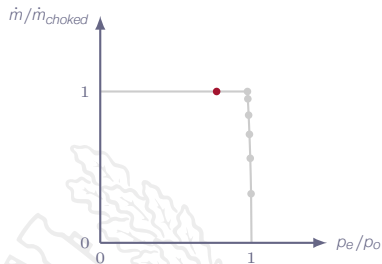
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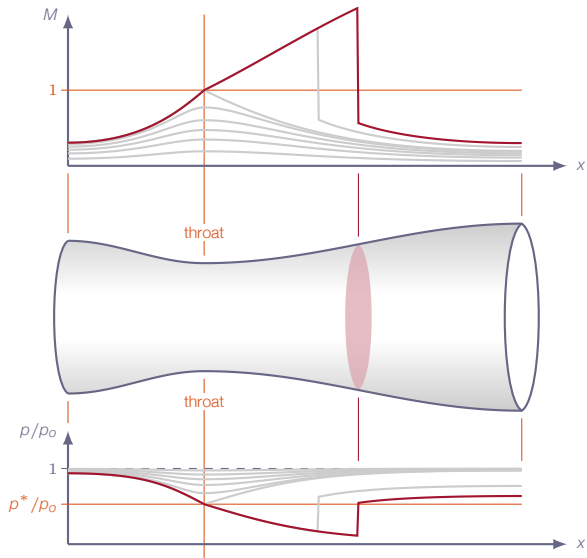
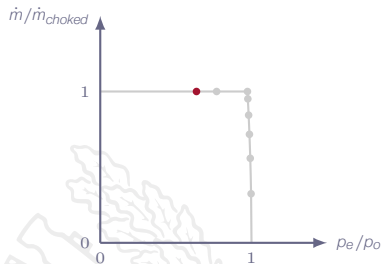
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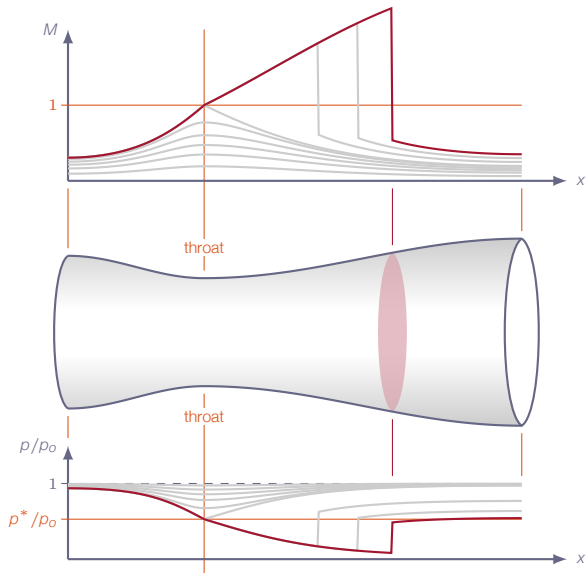
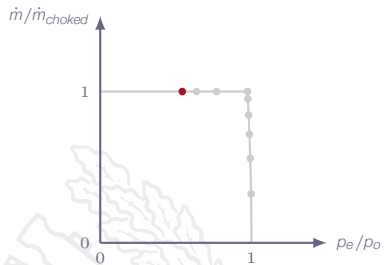
# Convergent-Divergent Nozzle



# Convergent-Divergent Nozzle

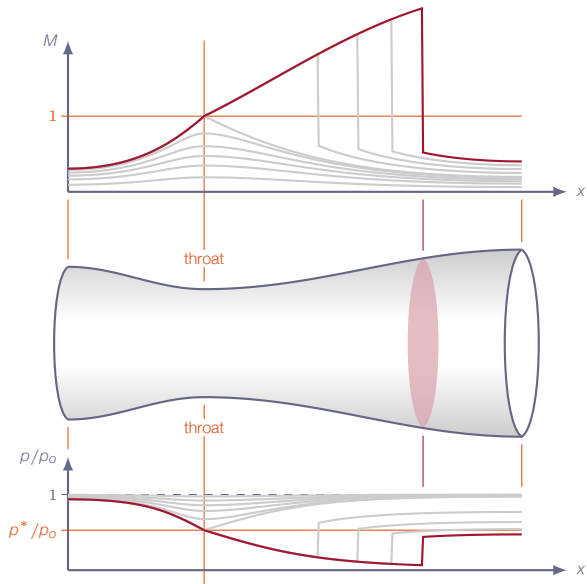
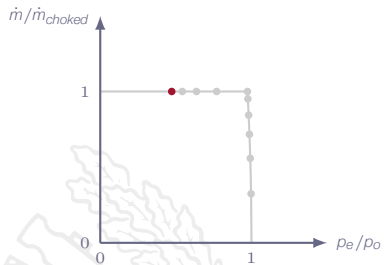


# Convergent-Divergent Nozzle

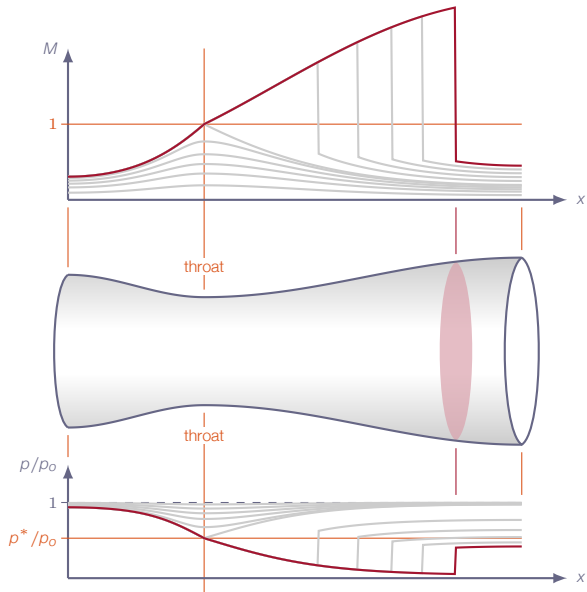
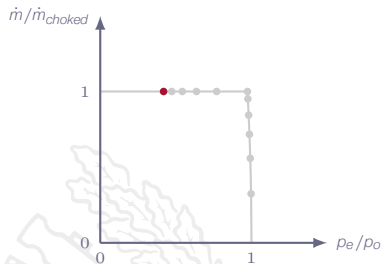




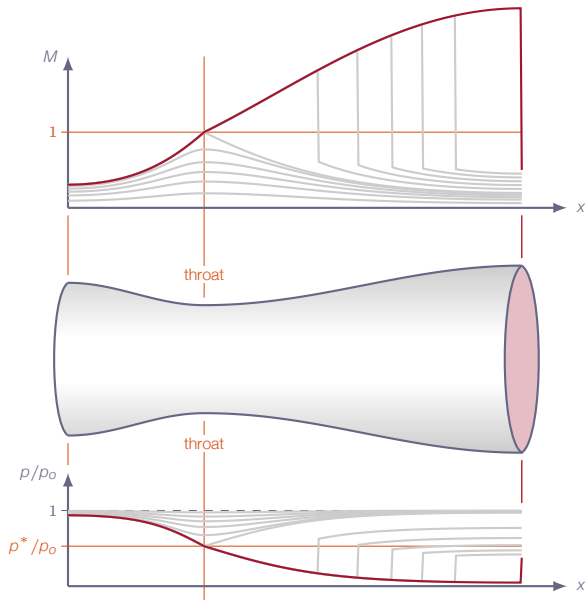
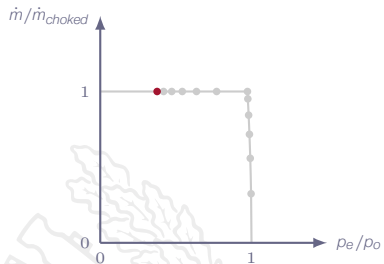
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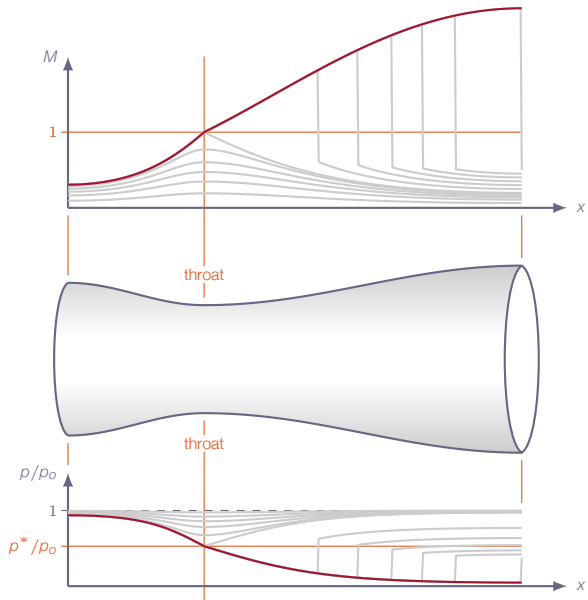
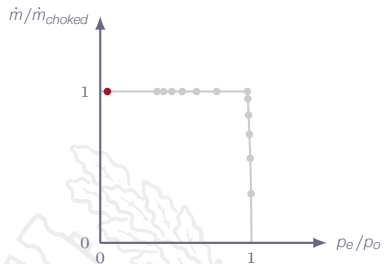
# Convergent-Divergent Nozzle



# Convergent-Divergent Nozzle



# Convergent-Divergent Nozzle



# Convergent-Divergent Nozzle



normal shock

$$\rho_o/\rho_e = (\rho_o/\rho_e)_{ne}$$

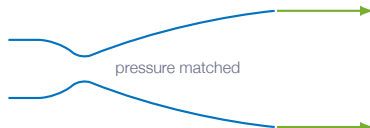
normal shock at nozzle exit



oblique shock

$$(\rho_o/\rho_e)_{ne} < \rho_o/\rho_e < (\rho_o/\rho_e)_{sc}$$

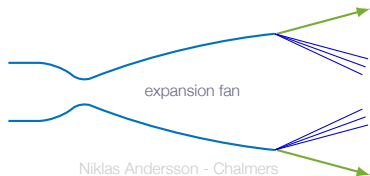
overexpanded nozzle flow



pressure matched

$$\rho_o/\rho_e = (\rho_o/\rho_e)_{sc}$$

pressure matched nozzle flow



expansion fan

$$\rho_o/\rho_e > (\rho_o/\rho_e)_{sc}$$

underexpanded nozzle flow

# Convergent-Divergent Nozzle

