

Lecture 14

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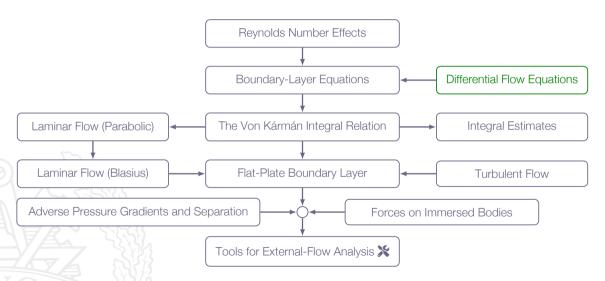


Learning Outcomes

- 4 Be **able to categorize** a flow and **have knowledge about** how to select applicable methods for the analysis of a specific flow based on category
- 6 Explain what a boundary layer is and when/where/why it appears
- **Explain** how the flat plate boundary layer is developed (transition from laminar to turbulent flow)
- **Explain** and use the Blasius equation
- **Define** the Reynolds number for a flat plate boundary layer
- **Explain** what is characteristic for a turbulent flow
- **Explain** flow separation (separated cylinder flow)
- **Explain** how to delay or avoid separation
- **Derive** the boundary layer formulation of the Navier-Stokes equations
- 32 Understand and explain displacement thickness and momentum thickness
- **Understand**, **explain** and **use** the concepts drag, friction drag, pressure drag, and lift

Let's take a deep dive into boundary-layer theory

Roadmap - Flow Past Immersed Bodies



Complementary Course Material

These lecture notes covers chapter 7 in the course book and additional course material that you can find in the following documents

MTF053_Equation-for-Boundary-Layer-Flows.pdf

 ${\tt MTF053_Turbulence.pdf}$



External Flow

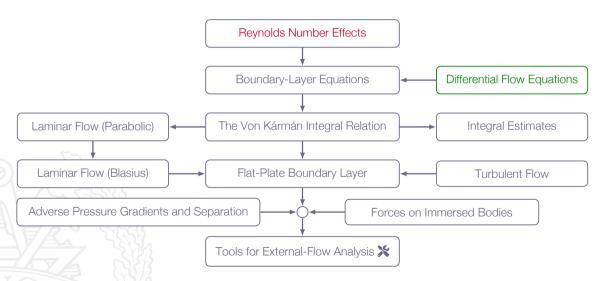
Significant viscous effects near the surface of an immersed body

Nearly inviscid far from the body

Unconfined - boundary layers are free to grow

Most often CFD or experiments are needed to analyze an external flow unless the geometry is very simple

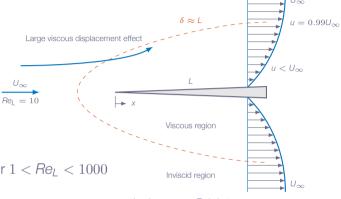
Roadmap - Flow Past Immersed Bodies

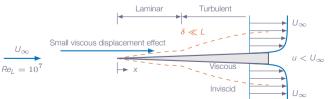


Reynolds Number Effects

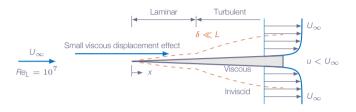


Note: no simple theory exists for $1 < Re_l < 1000$





Reynolds Number Effects



$$\frac{\delta}{x} \approx \begin{cases} \frac{5.0}{\text{Re}_{\text{X}}^{1/2}} & \text{laminar} & 10^3 < \text{Re}_{\text{X}} < 10^6 \end{cases}$$

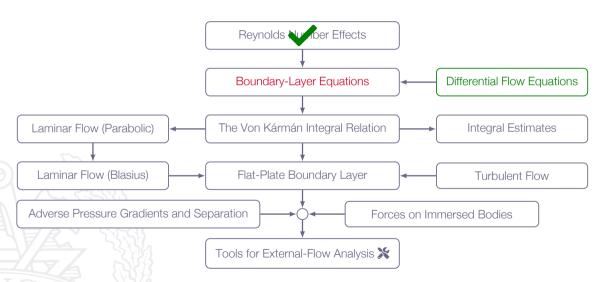
$$Re_{\text{L}} = \frac{U_{\infty} L}{\nu}$$

$$\frac{0.16}{\text{Re}_{\text{X}}^{1/7}} & \text{turbulent} & 10^6 < \text{Re}_{\text{X}} \end{cases}$$

$$Re_{\text{X}} = \frac{U_{\infty} x}{\nu}$$

Note! Re_{L} and the **local Reynolds number** Re_{x} are not the same if $L \neq x$

Roadmap - Flow Past Immersed Bodies



We will derive a set of equations suitable for **boundary-layer flow analysis**

Starting point: the **non-dimensional equations** derived in Chapter 5

We will assume two-dimensional, incompressible, steady-state flow

We will do an **order-of-magnitude** comparison of all the terms in the governing equations on non-dimensional form and identify terms that can be neglected in a **thin-boundary-layer** flow



The governing equations for two-dimensional, laminar, incompressible and steady-state flow with negligible body forces:

continuity:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

x-momentum:

$$\rho\left(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}\right) = -\frac{\partial \rho}{\partial x} + \mu\left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}\right)$$

y-momentum:

$$\rho\left(u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y}\right) = -\frac{\partial \rho}{\partial y} + \mu\left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2}\right)$$



$$x^* = \frac{x}{L}$$
 $y^* = \frac{y}{L}$ $u^* = \frac{u}{U_{\infty}}$ $v^* = \frac{v}{U_{\infty}}$ $\rho^* = \frac{\rho}{\rho U_{\infty}^2}$

continuity:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$\frac{\partial (u^* \mathbf{U}_{\infty})}{\partial (x^* L)} + \frac{\partial (v^* \mathbf{U}_{\infty})}{\partial (y^* L)} = \frac{\mathbf{U}_{\infty}}{L} \left(\frac{\partial u^*}{\partial x^*} + \frac{\partial v^*}{\partial y^*} \right) = 0$$



$$x^* = \frac{x}{L}$$
 $y^* = \frac{y}{L}$ $u^* = \frac{u}{U_{\infty}}$ $v^* = \frac{v}{U_{\infty}}$ $p^* = \frac{p}{\rho U_{\infty}^2}$

x-momentum:

$$\rho\left(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}\right) = -\frac{\partial \rho}{\partial x} + \mu\left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}\right)$$

$$\rho\left(u^* \frac{\mathbf{U}_{\infty}}{\partial(x^*L)} \frac{\partial(u^* \frac{\mathbf{U}_{\infty}}{\partial x^*L})}{\partial(x^*L)} + v^* \frac{\mathbf{U}_{\infty}}{\partial x^*L} \frac{\partial(u^* \frac{\mathbf{U}_{\infty}}{\partial x^*L})}{\partial x^*L}\right) = -\frac{\partial(\rho^* \rho U_{\infty}^2)}{\partial(x^*L)} + \mu\left(\frac{\partial^2(u^* \frac{\mathbf{U}_{\infty}}{\partial x^*L})}{\partial(x^*L)^2} + \frac{\partial^2(u^* \frac{\mathbf{U}_{\infty}}{\partial x^*L})}{\partial(x^*L)^2}\right)$$



$$\frac{\rho U_{\infty}^{2}}{L} \left(u^{*} \frac{\partial u^{*}}{\partial x^{*}} + v^{*} \frac{\partial u^{*}}{\partial y^{*}} \right) = -\frac{\rho U_{\infty}^{2}}{L} \frac{\partial \rho^{*}}{\partial x^{*}} + \frac{\mu U_{\infty}}{L^{2}} \left(\frac{\partial^{2} u^{*}}{\partial x^{*^{2}}} + \frac{\partial^{2} u^{*}}{\partial y^{*^{2}}} \right)$$

$$u^* \frac{\partial u^*}{\partial x^*} + v^* \frac{\partial u^*}{\partial y^*} = -\frac{\partial p^*}{\partial x^*} + \frac{\mu}{\rho U_{\infty} L} \left(\frac{\partial^2 u^*}{\partial x^{*2}} + \frac{\partial^2 u^*}{\partial y^{*2}} \right)$$

$$u^* \frac{\partial u^*}{\partial x^*} + v^* \frac{\partial u^*}{\partial y^*} = -\frac{\partial p^*}{\partial x^*} + \frac{1}{Re_L} \left(\frac{\partial^2 u^*}{\partial x^{*2}} + \frac{\partial^2 u^*}{\partial y^{*2}} \right)$$

Non-dimensional Flow Equations - Summary



continuity:

$$\frac{\partial u^*}{\partial x^*} + \frac{\partial v^*}{\partial y^*} = 0$$

x-momentum:

$$u^*\frac{\partial u^*}{\partial x^*} + v^*\frac{\partial u^*}{\partial y^*} = -\frac{\partial p^*}{\partial x^*} + \frac{1}{\textit{Re}_L}\left(\frac{\partial^2 u^*}{\partial x^{*2}} + \frac{\partial^2 u^*}{\partial y^{*2}}\right)$$

y-momentum:

$$u^* \frac{\partial v^*}{\partial x^*} + v^* \frac{\partial v^*}{\partial y^*} = -\frac{\partial p^*}{\partial y^*} + \frac{1}{Re_L} \left(\frac{\partial^2 v^*}{\partial x^{*2}} + \frac{\partial^2 v^*}{\partial y^{*2}} \right)$$

$$x^* = \frac{x}{L}$$

$$y^* = \frac{y}{L}$$

$$u^* = \frac{u}{U_{\infty}}$$

$$v^* = \frac{v}{U_{\infty}}$$

$$p^* = \frac{p}{\rho U_{\infty}^2}$$

$$Re_L = \frac{U_{\infty}L}{v}$$

To be able to find the relative sizes of different terms in the equations, we will first have a look at the flow parameters and operators

$$u^* = u/U_{\infty} \sim 1$$

$$x^* = x/L \sim 1$$

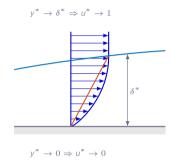
$$y^* = y/L \sim \delta^*$$

 δ denotes boundary layer thickness and $\delta^* = \delta/L$

Note! here, u^* is **not** the friction velocity and δ^* is **not** the displacement thickness

What about derivatives?

$$\frac{\partial u^*}{\partial y^*} \sim \frac{1-0}{\delta^*} = \frac{1}{\delta^*}$$



What about derivatives?

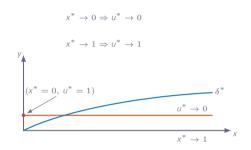
$$\frac{\partial u^*}{\partial y^*} \sim \frac{1-0}{\delta^*} = \frac{1}{\delta^*}$$

$$\frac{\partial^2 u^*}{\partial y^{*2}} = \frac{\partial}{\partial y^*} \frac{\partial u^*}{\partial y^*} \sim \frac{|0 - 1/\delta^*|}{\delta^*} = \frac{1}{\delta^{*2}}$$

$$y^* \to \delta^* \Rightarrow u^* \to 1, \frac{\partial u^*}{\partial y^*} \to 0$$

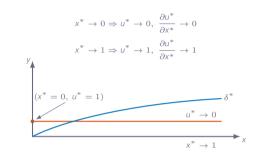
$$y^* \to 0 \Rightarrow u^* \to 0, \frac{\partial u^*}{\partial y^*} \to \frac{1}{\delta^*}$$

$$\frac{\partial u^*}{\partial x^*} \sim \frac{|0-1|}{1-0} = 1$$



$$\frac{\partial u^*}{\partial x^*} \sim \frac{|0-1|}{1-0} = 1$$

$$\frac{\partial^2 u^*}{\partial x^{*2}} = \frac{\partial}{\partial x^*} \frac{\partial u^*}{\partial x^*} \sim \frac{1-0}{1-0} = 1$$

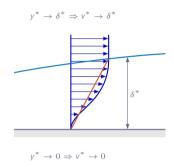


continuity:

$$\underbrace{\frac{\partial u^*}{\partial x^*}}_{\sim \frac{1}{1}} + \underbrace{\frac{\partial v^*}{\partial y^*}}_{\sim \frac{?}{\delta^*}} = 0 \Rightarrow v^* \sim \delta^*$$

 $\frac{\partial v^*}{\partial y^*}$ must be of the same order of magnitude as $\frac{\partial u^*}{\partial x^*}$ in order to fulfill the continuity equation

$$\frac{\partial v^*}{\partial y^*} \sim \frac{\delta^*}{\delta^*} = 1$$



$$\frac{\partial v^*}{\partial y^*} \sim \frac{\delta^*}{\delta^*} = 1$$

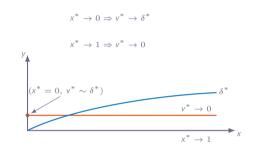
$$\frac{\partial^2 v^*}{\partial y^{*2}} = \frac{\partial}{\partial y^*} \frac{\partial v^*}{\partial y^*} \sim \frac{|0-1|}{\delta^*} = \frac{1}{\delta^*}$$

$$y^* \to \delta^* \Rightarrow v^* \to \delta^*, \frac{\partial v^*}{\partial y^*} \to 0$$

$$\delta^*$$

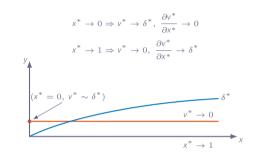
$$y^* \to 0 \Rightarrow v^* \to 0, \frac{\partial v^*}{\partial x^*} \to 1$$

$$\frac{\partial V^*}{\partial X^*} \sim \frac{|0 - \delta^*|}{1 - 0} = \delta^*$$



$$\frac{\partial V^*}{\partial X^*} \sim \frac{|0 - \delta^*|}{1 - 0} = \delta^*$$

$$\frac{\partial^2 v^*}{\partial x^{*2}} = \frac{\partial}{\partial x^*} \frac{\partial v^*}{\partial x^*} \sim \frac{\delta^* - 0}{1 - 0} = \delta^*$$



x-momentum:

$$\underbrace{u^* \frac{\partial u^*}{\partial x^*}}_{\sim 1 \times 1 = 1} + \underbrace{v^* \frac{\partial u^*}{\partial y^*}}_{\sim \delta^* \frac{1}{\delta^*} = 1} = -\frac{\partial p^*}{\partial x^*} + \frac{1}{Re_L} \left(\underbrace{\frac{\partial^2 u^*}{\partial x^{*2}}}_{\sim 1} + \underbrace{\frac{\partial^2 u^*}{\partial y^{*2}}}_{\sim \frac{1}{\delta^*} = 2} \right)$$

the boundary layer is assumed to be very thin $\Rightarrow \delta^* \ll 1$ and thus

$$\frac{\partial^2 u^*}{\partial x^{*2}} \ll \frac{\partial^2 u^*}{\partial y^{*2}}$$

assuming the inertial forces to be of the same size as the friction forces in the boundary layer we get: $1/Re_L \sim \delta^{*2}$

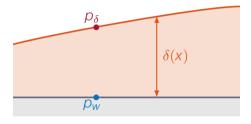
y-momentum:

$$\underbrace{U^* \frac{\partial V^*}{\partial X^*}}_{\sim 1 \times \delta^* = \delta^*} + \underbrace{V^* \frac{\partial V^*}{\partial y^*}}_{\sim \delta^* \frac{\delta^*}{\delta^*} = \delta^*} = -\frac{\partial p^*}{\partial y^*} + \underbrace{\frac{1}{Re_L}}_{\sim \delta^{*2}} \left(\underbrace{\frac{\partial^2 V^*}{\partial x^{*2}}}_{\sim \delta^*} + \underbrace{\frac{\partial^2 V^*}{\partial y^{*2}}}_{\sim \delta^*} \right)$$

examining the equation we see that all terms are at most of size $\delta^* \Rightarrow \frac{\partial \rho^*}{\partial y^*} \sim \delta^*$

 δ^* is small $\Rightarrow p$ is independent of y

The pressure can be assumed to be constant in the vertical direction through the boundary layer and thus p = p(x)



$$|\boldsymbol{\rho_{\delta}^*} - \boldsymbol{\rho_{w}^*}| \approx \frac{\partial \boldsymbol{\rho}^*}{\partial \boldsymbol{v}^*} \delta^* \sim \delta^{*2}$$

With the knowledge gained, we now move back to the dimensional equations

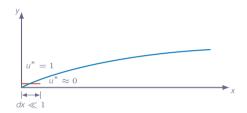
laminar

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial x} + v\frac{\partial^2 u}{\partial y^2}$$

turbulent

$$\begin{split} &\frac{\partial \overline{u}}{\partial x} + \frac{\partial \overline{v}}{\partial y} = 0\\ &\overline{u}\frac{\partial \overline{u}}{\partial x} + \overline{v}\frac{\partial \overline{u}}{\partial y} = -\frac{1}{\rho}\frac{d\overline{\rho}}{dx} + \nu\frac{\partial^2 \overline{u}}{\partial y^2} - \frac{\partial}{\partial y}\overline{u'v'} \end{split}$$



Limitations

- 1. The boundary layer equations do not apply close to the start of the boundary layer where $\frac{\partial u^*}{\partial x^*}\gg 1$
- 2. The equations are derived assuming a thin boundary layer

The pressure derivative can be replaced with a velocity derivative

Outside of the boundary layer the flow is inviscid \Rightarrow we can use the Bernoulli equation

$$\rho + \frac{1}{2}\rho U_{\infty}^2 = const \Rightarrow \frac{d\rho}{dx} + \rho U_{\infty} \frac{dU_{\infty}}{dx} = 0 \Rightarrow -\frac{1}{\rho} \frac{d\rho}{dx} = U_{\infty} \frac{dU_{\infty}}{dx}$$

laminar boundary layer

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = U_{\infty}\frac{dU_{\infty}}{dx} + v\frac{\partial^{2}u}{\partial y^{2}}$$

Two equations and two unknowns ⇒ possible to solve ⊙

Note! the boundary layer equations can be used for curved surfaces if the boundary layer thickness δ is small compared to the curvature radius r

