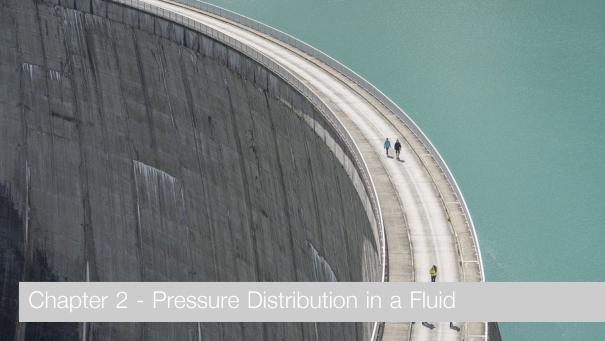


Lecture 3

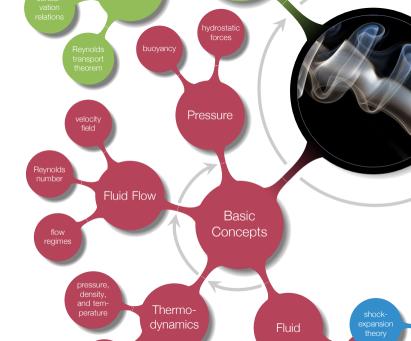
Niklas Andersson

Chalmers University of Technology Department of Mechanics and Maritime Sciences Division of Fluid Mechanics Gothenburg, Sweden

niklas.andersson@chalmers.se



Overview

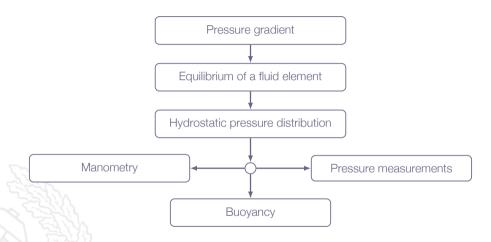


Learning Outcomes

- 9 Explain how to do a force balance for fluid element (forces and pressure gradients)
- 10 Understand and explain buoyancy and cavitation
- 11 **Solve** problems involving hydrostatic pressure and buoyancy

we will have a look at the pressure distribution in a fluid at rest, i.e. no flow yet...

Roadmap - Pressure Distribution in a Fluid



Motivation

Many problems does not include fluid motion

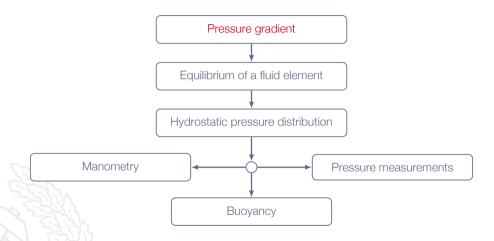
pressure distribution in a static fluid such as the pressure in the atmosphere or in oceans

pressure on solid surfaces due to presence of static fluid

floating and submerged bodies

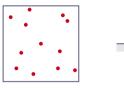


Roadmap - Pressure Distribution in a Fluid



Pressure

Pressure is a thermodynamic property





Pressure is not a force and has no direction

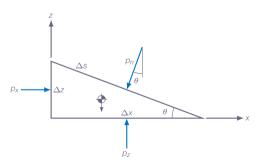
Forces arise when the molecules of the fluid interacts with the surface of an immersed body

A force in the surface-normal direction is generated due to the collision of fluid molecules and the surface

Fluid at rest - no shear (by definition)

Pressures p_x , p_z , and p_n may be different

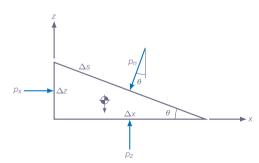
Small element ⇒ constant pressure on each face



$$\sum F_{x} = 0 = p_{x}b\Delta z - p_{n}b\Delta s \sin\theta$$

$$\sum F_z = 0 = \rho_z b \Delta x - \rho_n b \Delta s \cos \theta - \frac{1}{2} \rho g b \Delta x \Delta z$$

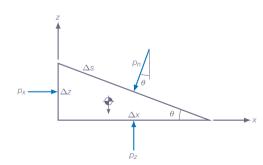
$$\begin{cases} \Delta z = \Delta \sin \theta \\ \Delta x = \Delta \sin \theta \end{cases}$$



$$\sum F_{x} = 0 = p_{x}b\Delta z - p_{n}b\Delta z$$

$$\sum F_z = 0 = \rho_z b \Delta x - \rho_n b \Delta x - \frac{1}{2} \rho g b \Delta x \Delta z$$

$$\begin{cases} \rho_{X} = \rho_{n} \\ \rho_{Z} = \rho_{n} + \frac{1}{2}\rho g \Delta z \end{cases}$$



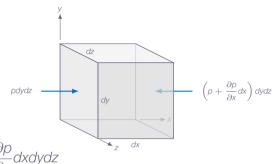
Since θ is arbitrary, the result is general

There is no pressure change in the horizontal direction

The pressure change in the vertical direction is proportional to the depth

"The pressure in a static fluid is a point property, independent of orientation"

Pressure Forces on a Fluid Element



$$p = p(x, y, z, t)$$

$$dF_x = pdydz - \left(p + \frac{\partial p}{\partial x}dx\right)dydz = -\frac{\partial p}{\partial x}dxdydz$$

$$dF_{p} = -\left[\frac{\partial p}{\partial x}\mathbf{e}_{x} + \frac{\partial p}{\partial y}\mathbf{e}_{y} + \frac{\partial p}{\partial z}\mathbf{e}_{z}\right]dxdydz$$

$$\mathbf{f}_{p} = -\nabla p$$

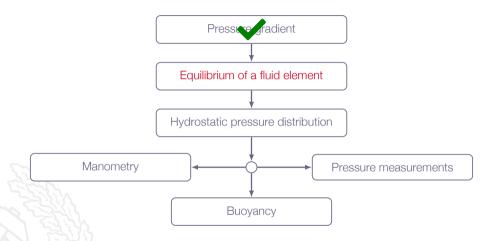
f is the net force per unit volume

Pressure Forces on a Fluid Element

"it is not the pressure but the pressure gradient causing a net force which must be balanced by gravity or acceleration"



Roadmap - Pressure Distribution in a Fluid



Equilibrium of a Fluid Element

Force balance for a small element

pressure gradients gives surface forces

body forces (electromagnetic or gravitational potentials)

surface forces due to viscous stresses

Newton's second law:

$$\sum \mathbf{f} = \mathbf{f}_{\rho} + \mathbf{f}_{g} + \mathbf{f}_{v} = -\nabla \rho + \rho \mathbf{g} + \mathbf{f}_{v} = \rho \mathbf{a}$$

Equilibrium of a Fluid Element

Hydrostatic problems:

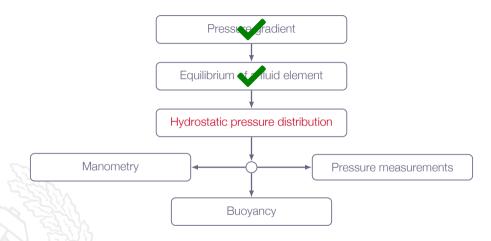
- 1. no viscous forces
- 2. no acceleration

Newton's second law reduces to:

$$\nabla p = \rho \mathbf{g}$$

(the general form of Newton's second law will be studied later)

Roadmap - Pressure Distribution in a Fluid



$$\nabla p = \rho \mathbf{g}$$

 ∇p is perpendicular everywhere to surfaces of constant p

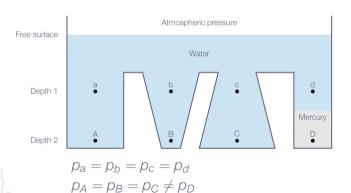
The normal of constant-pressure surfaces will be aligned with $\ensuremath{\mathbf{g}}$

$$\mathbf{g} = -g\mathbf{e}_{z}$$

$$\frac{dp}{dz} = -\rho g$$

$$p_2 - p_1 = -\int_1^2 \rho g dz$$

for liquids, we assume constant density
$$\Rightarrow p_2 - p_1 = -\int_1^2 \rho g dz = -\rho g(z_2 - z_1)$$



Is the incompressible assumption for liquids a good assumption?

the density is 4.6 percent higher at the deepest part of the ocean - so yes!

$$\rho_2 - \rho_1 = -\int_1^2 \rho g dz = -\rho g(z_2 - z_1)$$

$$\rho_2 - \rho_1 = -\int_1^2 \rho g dz = -\rho g(z_2 - z_1)$$

Why is mercury used for pressure measurements?

Hydrostatic Pressure in Gases

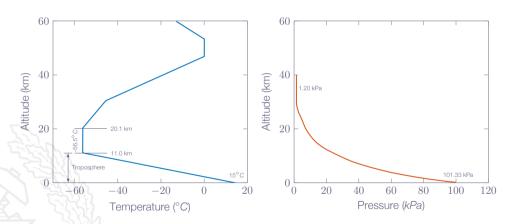
$$\frac{dp}{dz} = -\rho g = -\frac{p}{RT}g$$

both pressure and temperature varies with altitude

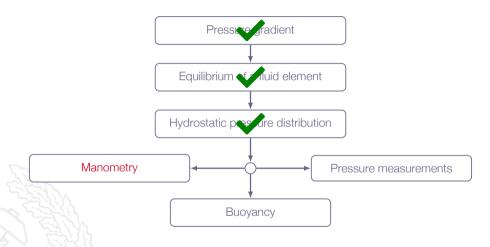
$$\int_{1}^{2} \frac{dp}{p} = \ln \frac{p_2}{p_1} = -\frac{g}{R} \int_{1}^{2} \frac{dz}{T}$$

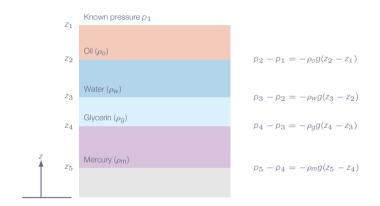
Temperature variation T(z) needed

Hydrostatic Pressure in Gases



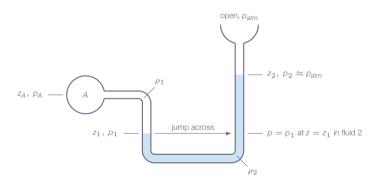
Roadmap - Pressure Distribution in a Fluid





$$\rho_5 - \rho_1 = -\rho_m g(z_5 - z_4) - \rho_g g(z_4 - z_3) - \rho_w g(z_3 - z_2) - \rho_o g(z_2 - z_1)$$

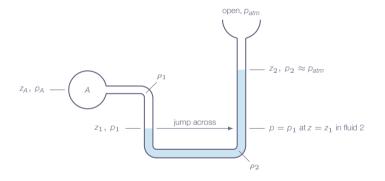
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Pascal's law:

"Any two points at the same elevation in a continuous mass of the same static fluid will be at the same pressure"

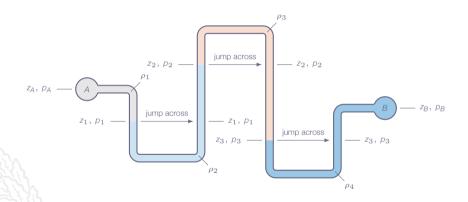
$$\rho_A + \rho_1 g(z_A - z_1) - \rho_2 g(z_2 - z_1) = \rho_2 \approx \rho_{atm}$$



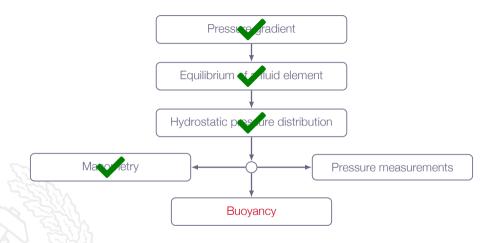
Pascal's law:

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Roadmap - Pressure Distribution in a Fluid



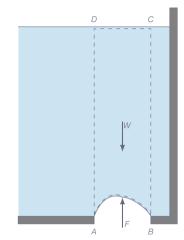


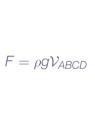


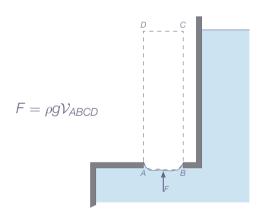
Archimedes:

A body immersed in a fluid experiences a vertical buoyant force equal to the **weight of the fluid it displaces**

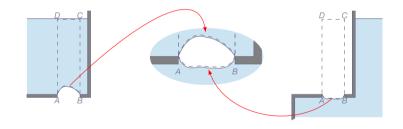
A floating body displaces its own weight in the fluid in which it floats





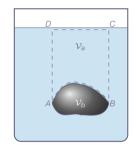






$$F_{up} = \rho g(\mathcal{V}_a + \mathcal{V}_b)$$

$$F_{down} = \rho g \mathcal{V}_a$$





In general

$$\mathbf{F}_B = \sum \rho_i g(displacement\ volume)_i$$

Floating bodies

$$\mathbf{F}_B = body \ weight$$

Buoyancy - Stability

Center of gravity *G*Center of buoyancy *B*Symmetry line
Metacenter *M*

small disturbance

line of symmetry

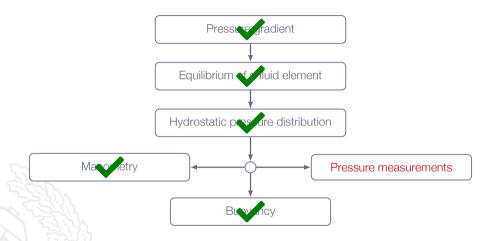
Note! the center of buoyancy (B) is, in this case, the centroid of the displaced volume of liquid

small disturbance

Buoyancy - Stability



Roadmap - Pressure Distribution in a Fluid

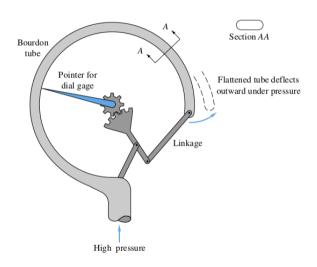


Pressure measurement

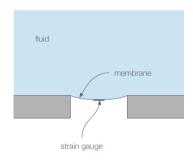
Pressure is a derived property

The force per unit area related to fluid molecular bombardment of a surface

Pressure measurement

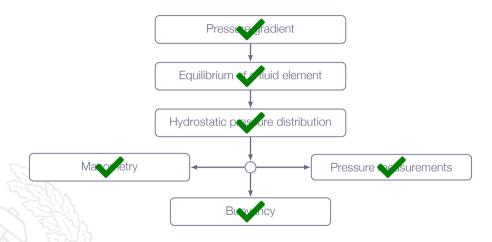


Pressure measurement





Roadmap - Pressure Distribution in a Fluid



Manometer Example

$$p_1 + \sum_{down} \rho_i g \Delta_i - \sum_{up} \rho_i g \Delta_i = p_2$$

$$p_1 + (\Delta_2 + \Delta_1) \rho_A g - \Delta_1 \rho_B g - (\Delta_2 + \Delta_3) \rho_A g = p_2$$

$$\downarrow^{\Delta_2}$$

$$\uparrow^{\Delta_1}$$

$$\left(\frac{\rho_1}{\rho_A g} + z_1\right) - \left(\frac{\rho_2}{\rho_A g} + z_2\right) = \Delta_1 \left(\frac{\rho_B}{\rho_A} - 1\right)$$

 $\rho_1 + (\Delta_2 + \Delta_1)\rho_A g - \Delta_1 \rho_B g - (\Delta_2 + \mathbf{Z_2} - \mathbf{Z_1})\rho_A g = \rho_2$

Iceberg Efficiency





OUR NEXT-GENERATION FOAM-FILLED ICEBERG ACHIEVES NEAR-IOO% EFFICIENCY, FLOATING ALMOST ENTIRELY ABOVE THE OCEAN SURFACE.



"BUT WAIT," YOU MIGHT BE THINKING. "HOU VILL SUCH A LIGHTUFIGHT ICEBERS POSE A THREAT TO HUBRISTIC OCEAN LINERS?" THAT'S WHERE THE TORPEDOES COME IN.

I'M SORRY WHAT PROJECT



SECURITY?